



Corrosion Control Treatment: Lessons Learned from the Field

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Lessons

- Source changes require re-evaluation of corrosion treatment
- Changes in treatment can affect lead & copper corrosion
- Just because the system is “optimized” does not mean there are no corrosion issues
- All plumbers are not created equal
- Pay attention to the NaOH injection point design



Lesson 1: Changing Sources Require Re-evaluation of Corrosion Control Treatment

- ◆ Central Arizona Project
- ◆ South Tahoe PUD, CA
- ◆ Lake Stevens, WA
- ◆ Longview, WA
- ◆ Manteca, CA
- ◆ Flint, MI

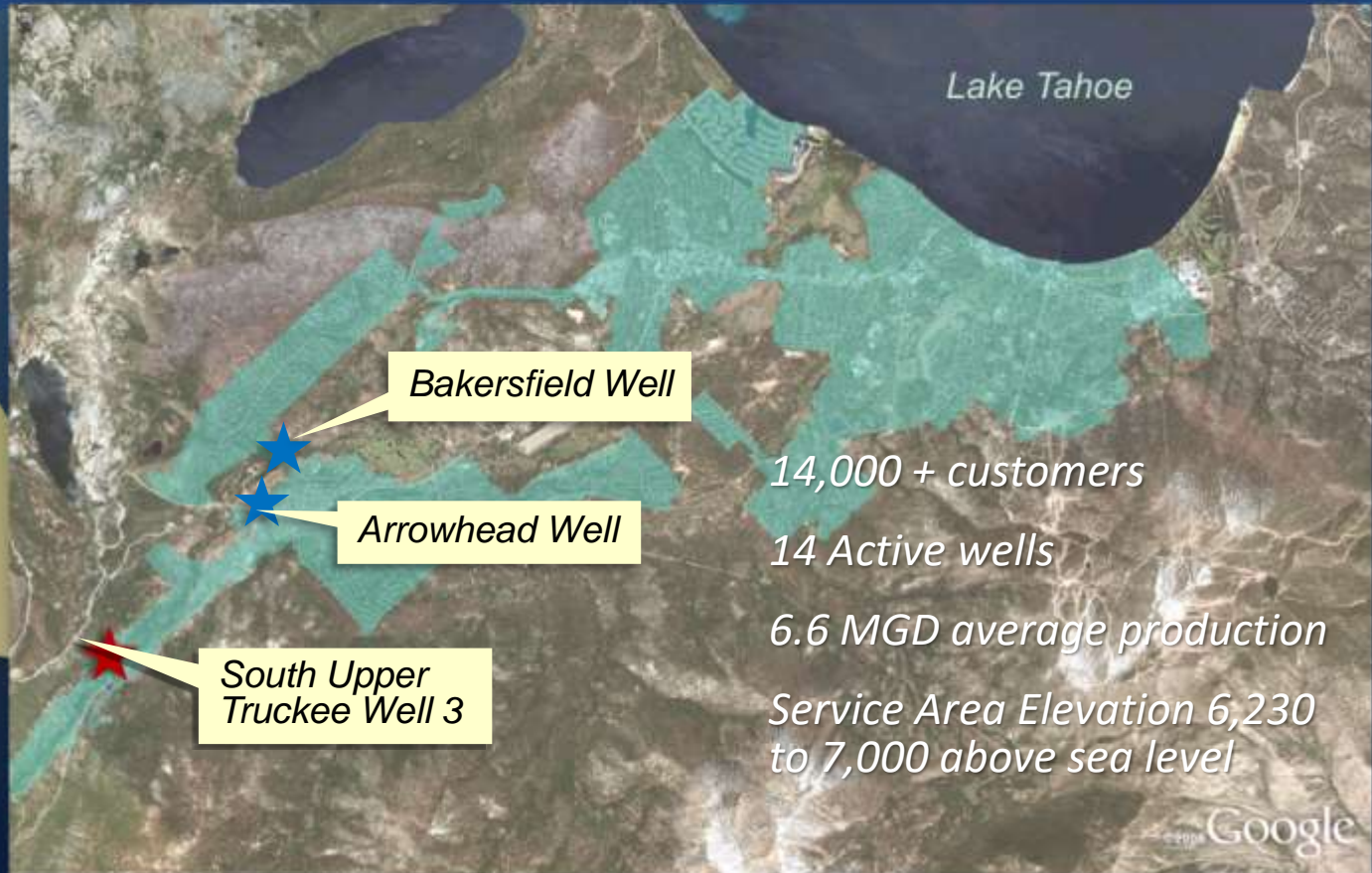


Central Arizona Project

- Tucson
 - Historically used groundwater
 - Imported surface water from CAP
- Destabilized scale on the pipe wall
- Vote to not allow CAP water into system
- Substantial \$ spent on corrosion control evaluations and treatment
- CAP water used for ASR



S Tahoe PUD Location Map



Arsenic Compliance Plan

- Arrowhead & Bakersfield Wells
 - Reduce their production
 - Provide arsenic treatment
- S Upper Truckee Wellfield
 - Increase production
 - Treat to reduce water's corrosivity



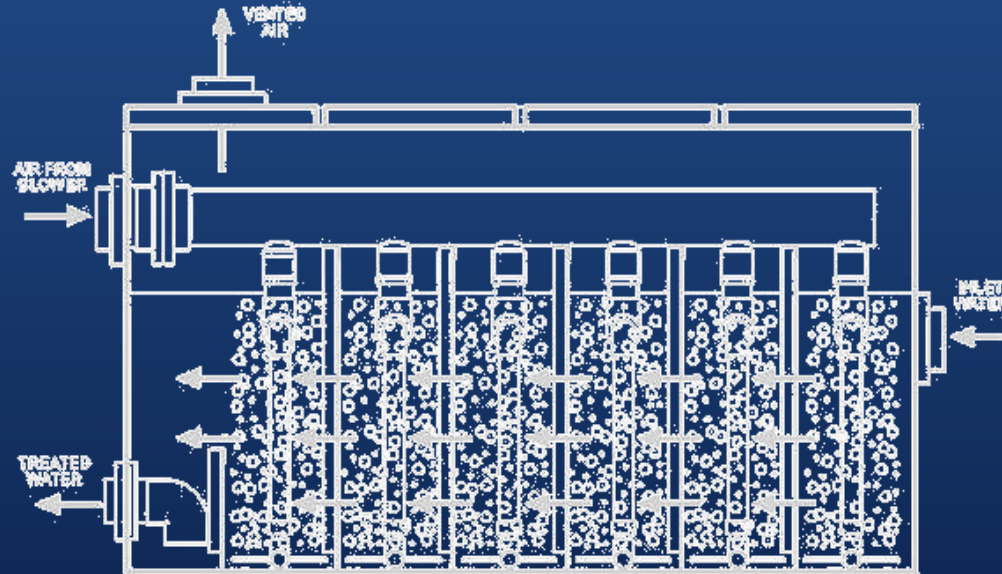
Corrosion Concerns Christmas Valley Pressure Zone

- ◆ Lead & Copper Rule Monitoring (system wide)
 - ◆ 90th percentile lead – 6.4 $\mu\text{g/l}$
 - ◆ 90th percentile copper – 0.48 mg/l
- ◆ 4 of 7 first draw tap samples exceeded 1.3 mg/l copper when the South Upper Truckee wells were in service
- ◆ Premature corrosion failures
 - ◆ Hot water heaters
 - ◆ Sand separator



Aeration Alternatives for pH Adjustment

- Low Profile Aeration
 - DeepBubble Multi-Stage Aeration
 - Shallow Tray Aeration
- Packed Tower Aeration
- Venturi Eductor CO₂ Stripping
- Multiple Tray Aeration
- Rotating Packed Bed Stripping



Pilot Testing

Goals

- Raise pH ≥ 7.5
- CO₂ ≤ 5 mg/l
- Rn-222 ≤ 300 pCi/l

Evaluate

- Copper - corrosion & leaching
- Lead-tin solder - corrosion & leaching
- Mild steel - corrosion & scale release
- Galvanized steel – corrosion & scale release



Pilot Aeration Unit

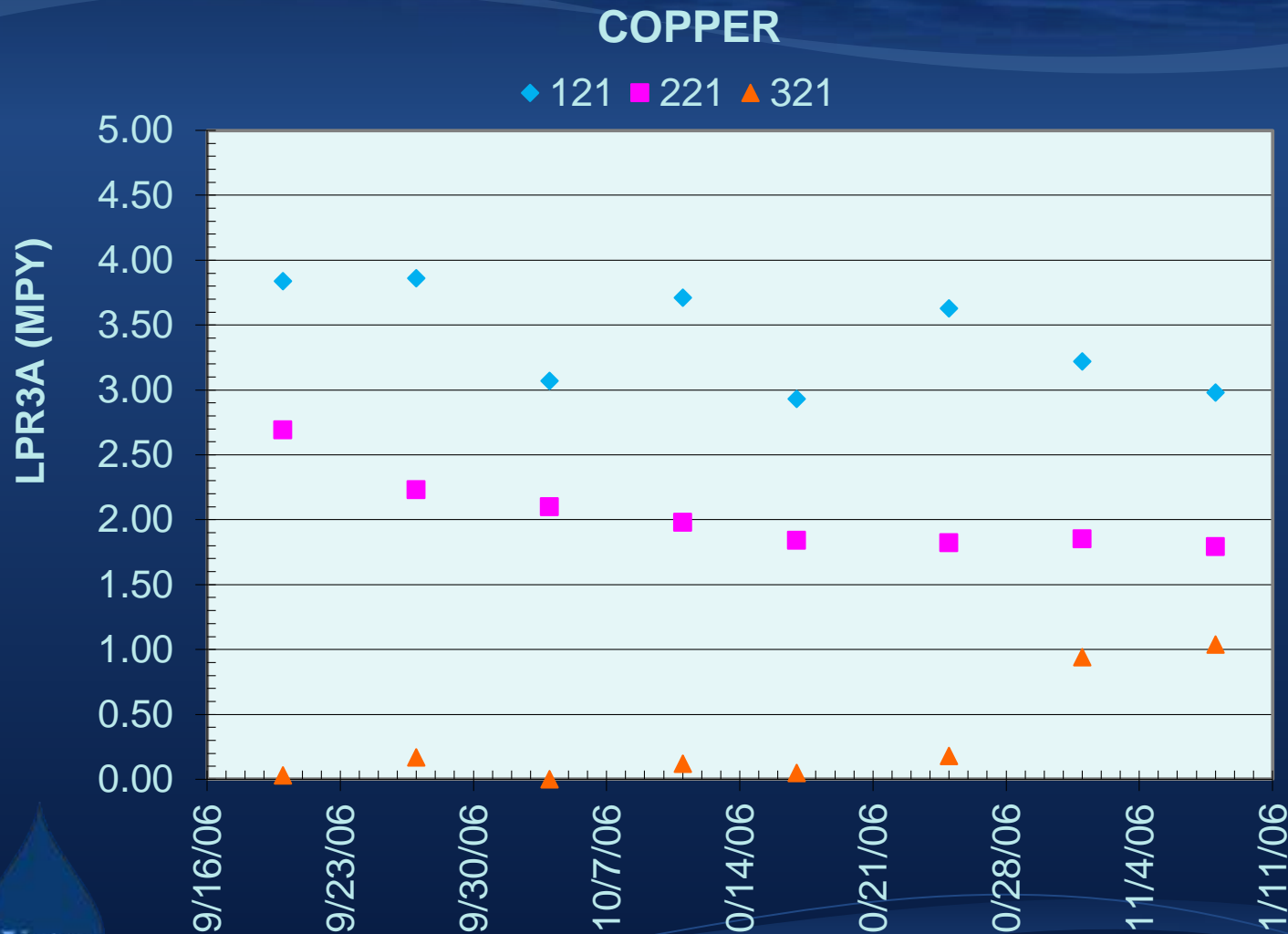
- ◆ Lowered Rn-222
 - ◆ Well water 462 pCi/l (median)
 - ◆ Aerated water 18 pCi/l (median)
- ◆ Stripped carbon dioxide to less than 5 mg/l
- ◆ Increased pH from 6.2-6.3 to 7.6
- ◆ Moderate increase in dissolved oxygen from 7.4 to 9.5 mg/l



Linear Polarization Probes & Copper Tubing



Linear Polarization Measurements: Copper



Findings: Copper Corrosion

- Aeration
 - ◆ Reduced copper corrosion 34%
 - ◆ Reduced first draw copper 30%
- Aeration plus sodium silicate
 - ◆ Reduced corrosion 83%
 - ◆ Reduced first draw copper 58%
 - ◆ Silicate addition was beneficial
- Uniform corrosion
- No pitting corrosion observed



Findings: Lead-Tin Solder Corrosion

- Aeration
 - ◆ Reduced lead-tin corrosion 90%
 - ◆ Reduced first draw lead >77%
 - ◆ Uniform corrosion with very slight pitting
- Aeration plus sodium silicate
 - ◆ Reduced lead-tin corrosion 52%
 - ◆ Reduced first draw lead >77%
 - ◆ Uniform corrosion with very slight pitting
 - ◆ Silicate addition not beneficial



Treatment Recommendations

- Provide low profile aeration for South Upper Truckee Well No. 3
- Provide room for 3 mg/l NaOH feed or sodium silicate
- Collect lead & copper tap samples after the facility has been on line 4-6 months



South Upper Truckee Well 3 Aeration Facility

- ◆ 2 DeepBubble Multi-Stage Aeration Units
- ◆ Results
 - ◆ Raised pH from 6.35 to 7.75
 - ◆ Reduced CO₂ from 30 mg/l to <2 mg/l
 - ◆ Reduced Rn from 589 pCi/l to 44 pCi/l
 - ◆ Christmas Valley tap samples (90th percentile)
 - Pb <2.5 µg/l
 - Cu 0.03 mg/l
 - ◆ Supplemental sodium hydroxide is not necessary



South Upper Truckee Well 3 Aeration Facility



Lake Stevens

- Everett water
 - ◆ Elevated DO: 11.0 mg/l
 - ◆ High ORP: 600
 - ◆ Soft, low alkalinity, low TDS water
- Lake Stevens well
 - ◆ Low DO: 0.5 mg/l
 - ◆ Low ORP: 350
 - ◆ Moderately hard, iron, manganese, H₂S, ammonia
- Groundwater introduced into area previously receiving surface water
 - ◆ Destabilized iron scale on galvanized steel and steel pipe
 - ◆ Leaks in unlined steel
 - ◆ PUD discontinued use of well as a result



Manteca, CA

- Originally 100% groundwater supply
- 2005 – Sierra surface water supply added
- Red water complaints
 - Manteca – pre 1970 galvanized services & plumbing
- No red water complaints
 - Tracy – Zn barrier coat
 - Lathrop – new community
- 90th percentile Pb & Cu
 - Virtually unchanged



Manteca, CA Surface Water

- Surface water: low TDS, high DO
- Ryzner Index: 9.3
 - >8 increasingly corrosive of iron & steel
 - >8.5 typical of red water conditions
- Cl⁻/SO₄⁻² mass ratio: 2.8
 - >0.58 increased galvanic corrosion
- Cl₂ residual: 1.2 mg/l at turnouts
 - > 0.8 mg/l increasing corrosive to steel



Manteca, CA

- Florist shop
 - Galvanized service
 - Received groundwater in morning
 - Received surface water in afternoon
 - pH varied 7.4 to 8.2
 - TDS varied 82 to 260 mg/l



Manteca Corrective Action

- ◆ Modify operation of S San Joaquin Irrigation District WTP
 - ◆ Initially operating at pH 8.0 & 40 mg/l alkalinity (lime & CO₂ addition)
 - ◆ Reduced CO₂ addition
 - ◆ Raised pH near 8.5
- ◆ Orthophosphate addition at turnouts
 - ◆ Not implemented



Lesson 2: Changes in treatment can effect lead & copper corrosion

● Washington, DC



Washington, DC

- Potomac River source of supply
- Conventional treatment with free Cl_2 residual
- 1992 – June 1994 initial LCR sampling exceeded Lead Action Level
- 1993-1996 TCR violations
- 1994 increased Cl_2 residual to 4 mg/l
 - ORP increased
 - Pb (II) scale oxidized to Pb (IV)
 - PbO_2 scales low solubility over wide pH range
- June 1997 optimum corrosion control $\text{LSI} > 0$



Washington, DC

- 1992-2004 seasonal pH fluctuation 7.0 to 8.9
- Feb 2000 optimum corrosion control pH
 - 7.7 ± 0.3 points of entry
 - 7.7 ± 0.3 distribution samples
- May 2002 optimum corrosion control pH
 - 7.4 to 7.8 points of entry
 - 7.0 distribution samples
 - Retroactive to July 2000
- Feb 2000 reduced tap monitoring



Washington, DC

- Nov 2000 converted to chloramine
 - ◆ Lower ORP from >650 mV to 450-500 mV
 - ◆ Pb (IV) scale reverted to Pb (II)
 - ◆ Pb (II) influenced by low and varying pH
- Exceeded Lead Action Level 2000 – 2004
 - ◆ 90th percentile 36 to 75 $\mu\text{g/l}$
 - ◆ 17 to 68% samples exceeded 15 $\mu\text{g/l}$
- Aug 2004
 - ◆ Orthophosphate addition
 - ◆ pH 7.7 ± 0.1 goal (± 0.3 enforceable)



Lesson 3: Just because the system is “optimized” does not mean that there are no corrosion issues

- Horizon House, Seattle – fire sprinkler & recirculation hot water system leaks
- Spokane VA Hospital – fire sprinkler leaks
- San Ramon, EBMUD – blue water
- Manteca, CA – red water
- Hollister Country Rose – blue water



Horizon House - Seattle

- Three Buildings Housing 450 Elderly Assisted Living Housing
- Buildings – 5 to 20 Years Old.
- Water Supply: LCR Optimized
 - pH – 8.0 - 8.2,
 - Alkalinity > 20 mg/l CaCO₃
- Problems:
 - Recirculating Hot Water Copper Pipe Pitting Failures
 - 10 - 15 years
 - Fire Sprinkler Water Supply Steel Pipe Pitting Failures
 - 15-20 years



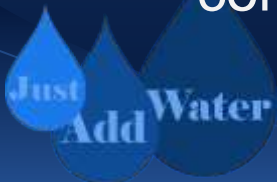
Horizon House

- Sink Sampling for Copper
 - ◆ Hot Water – 0.5 mg/L + 0.2 mg/l
 - ◆ Cold Water – 0.2 mg/l + 0.1 mg/l
- Corrective Measures:
 - ◆ Smaller hot water circulating pumps to lower velocity from 7 to 3 ½ FPS
 - ◆ Use Type L copper rather than Type M (increased wall thickness)
 - ◆ Phosphate corrosion pot feeders for fire sprinkler supply
 - ◆ Reduce frequency of fire sprinkler pipe flushing from weekly to monthly



EBMUD: San Ramon

- EBMUD optimized for corrosion control
- Source: S Bay Aqueduct
- Extended transmission main with new reservoir to serve developing area
- Water age
 - Lost chlorine residual
- ≈ 5,000 residences
- 40 - 50% blue water complaints



EBMUD: San Ramon

- Poorly adherent malachite scale
- Rechlorination station installed after the reservoir
- Building moratorium
- Developers sued EBMUD
- EBMUD sued insurance company
 - Battling experts
 - MIC
 - ORP
 - >\$10 million award



Conclusions:

- Changing treatment and water quality can destabilize corrosion scale
- Corrosion problems occur even when system has “optimized” per LCR
- Water quality and purveyor are often blamed
- Water purveyors need to carefully assess situation or liability can be substantial



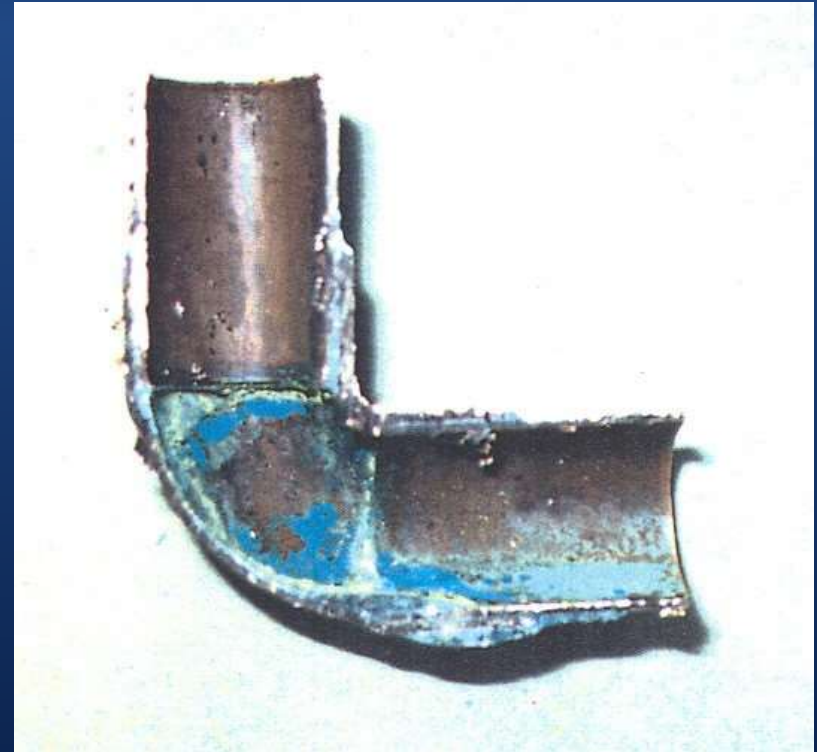
Lesson 4: All Plumbers Are Not Created Equal

- Duplex in Pierce County served by a groundwater
- The Hamilton, Palo Alto



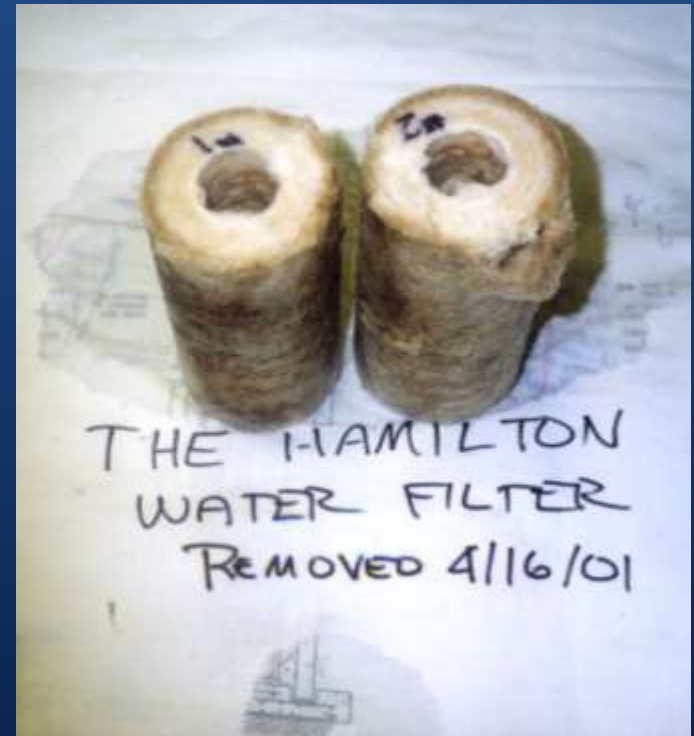
Pierce County Duplex

- First draw copper > 6 mg/l
- Concerned resident
- Attorneys got involved
- Plumbing samples collected
- Acidic flux runs



The Hamilton Apartments: Palo Alto

- ◆ 3-Year-old building housing
- ◆ 35 luxury residences for elderly
- ◆ Kitchen and dining room
- ◆ All copper piping
- ◆ Black greasy scum in tubs and sinks
- ◆ Particulate matter clogging faucets in a week
- ◆ Discoloration of kitchen cartridge filters in a week
- ◆ Plumber/contractor responsible under warranty



Excess Flux and Dirt Deposits in Luxury Apartment Residence – Palo Alto, CA



The Hamilton Water Quality Testing

Before – Chlorine Disinfection of
Apartment Complex Plumbing

	Cold Water	Hot Water
HPC	91 – 3700	3700 – 57,000
Coliform	1 Positive/4	0 Positive/3
Iron	1.35 mg/l	1.5 – 3.2 mg/l
Copper	1.6 mg/l	1.5 – 6.5 mg/l



The Hamilton – Water Quality Testing

After Chlorine Disinfection (200 mg/l for 3 hrs)

	Cold Water		Hot Water	
HPC	0 – 4	0 – 14	0 – 2	0 – 52
Coliform	0/14	1/14	0/14	0/4
Iron (mg/l)	< 0.05	0.10	< 0.05	0.15
Copper (mg/l)	0.01	0.05	0.07	0.10
pH	8.45	-	7.98	-



*The Hamilton – 3 Months After Chlorine Disinfection**

🔴 Tub Film Testing

- 💧 Petroleum hydrocarbons - 5.9%
- 💧 Copper - 2.3 mg/l
- 💧 Iron - 0.06 mg/l

**200 mg/l for 3 hours*



Corps of Engineers Hot Water Flushing Technique to Dissolve Excessive Flux

- Temperature: 160 – 180°F
- Velocity: > 7 FPS
- Time: 4 Hours
- Facilities Engineering Application Program
 - FEAP - TR – FM – 94109 – June 1994
- “Demonstration of a field rehabilitation technique for removing corrosive solder flux in cold water copper piping systems.”



Lesson 5: Pay attention to the NaOH Injection Point Design

- Pipeline immediately downstream of NaOH can have a pH significantly higher than the downstream distribution system
- Do not feed NaOH near a control valve
- Have a positive NaOH shutoff at the injector



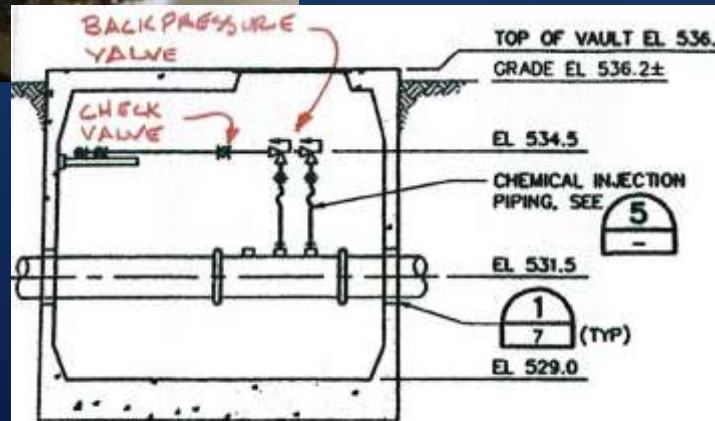
Do Not Feed NaOH in Front of a Control Valve



NaOH Injected Above the Pipe

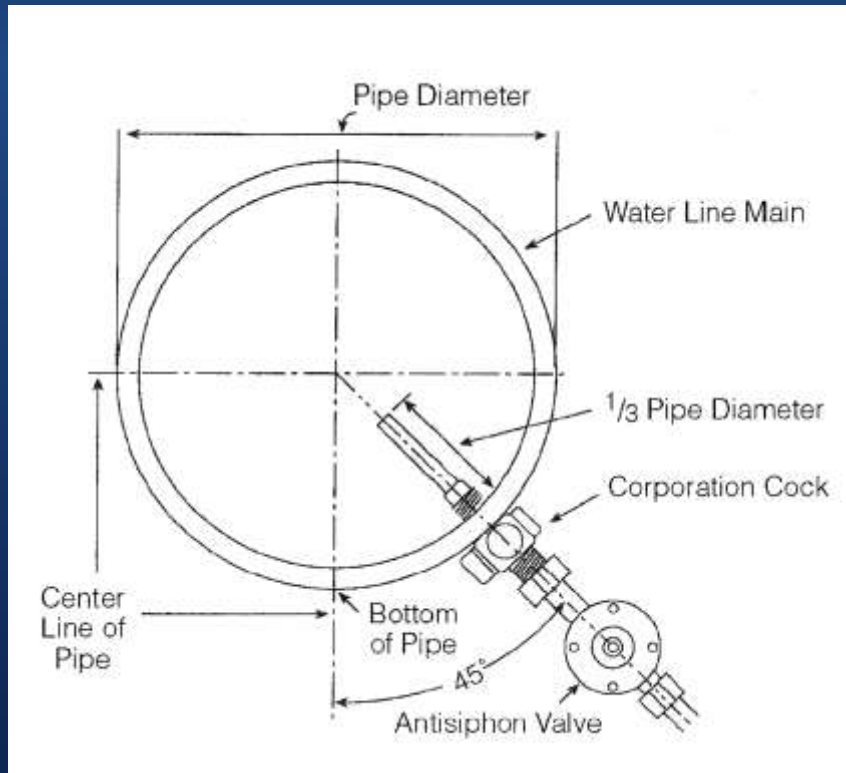


- NaOH may leak into water main when the well shuts down
- CaCO_3 precipitate will form in the pipe



INJECTION VAULT SECTION

Improved NaOH Injection



- Install the injector & NaOH piping below horizontal centerline
- Consider installing an electrically actuated ball valve near the injector interlocked with the well pump starter

Soften Carrier Water if Used



Questions

